

ORIGINAL RESEARCH ARTICLE

Influence of Soret and Radial Magnetic Field on Natural Convection of a Chemically Reactive Fluid in an Upright Porous Annulus.

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ABSTRACT

Mass fluxes produced by temperature gradients is known as the Soret or thermal-diffusion effect and this effect can be very crucial in the appearance of strong density difference in the flow premises. This article therefore explores the analytical solutions of natural convection of a chemical reacting fluid in the involvement of Soret and radial magnetic field in an annular upstanding permeable zone within concentric cylinders' $r = 1$ and $r = b$. The non-linear formulated equations that govern the flow are resolved by a semi-analytical approach. The consequences of the numerous governing controlling parameters embedded in the formulated model is thoroughly described with the use of illustrative plots. It is noteworthy to report that raising the levels of Frank–Kamenetskii, sustentation, and thermo-diffusion parameters increases fluid velocity whereas reducing the radial magnetic field effect weakens the fluid flow. Additionally, it is significant to report that the sheer stress on the annular walls can be effectively regulated by applying appropriate values of magnetic number. In conclusion, the variations of the key parameters in this study can be used more effectively to control heat transfer and fluid flow using an annular geometry. This study can find relevance in geothermal power generation, drilling activities, space vehicles technology and nuclear power plants etc.

ARTICLE HISTORY

Received June 29, 2023.

Accepted September 18, 2023.

Published September 30, 2023.

KEYWORDS

Natural convection, Chemically reactive fluid, Soret effect, Radial magnetic field, Vertical permeable annulus, Semi-analytical approach.



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INTRODUCTION

Researching the implications of heat and mass transfer across a chemically reacting fluids enclosed by various geometrical shapes is of particular interest to researchers attributed to its relevance to transpiration cooling of re-entry vehicles, rocket boosters and film vaporization in combustion chambers (Muthuraj and Srinivas, 2010). The simulation of chemical reacting fluids was first proposed by Frank Kamenetskii in 1969. As asserted by (Makinde 2008), most of lubricants utilized in industrial and technological operations, namely synthetic esters, polyphony lathers, hydrocarbon oils, polyglycols, and so forth, are reactive. With these concerns in mind, works of Hamza *et al.* (2023a, 2023b) recently shed more light on the implications of hydromagnetic natural convection of a chemically reacting fluid using homotopy perturbation technique. It is concluded from their results that mounting level of Frank-Kamenetskii, representing the viscous heating term is noticed to encourage both the thermal and

hydromagnetic fluid. Ojemer¹ and Onwubuya (2023) describe the analysis of steady mixed convection flow of Arrhenius-controlled chemical reaction and an exothermic fluid along an isothermally heated superhydrophobic microchannel due to heat source/sink. Ojemer¹ *et al.* (2023) focused their search on the analytical treatment of Arrhenius-controlled fluid in an upright microchannel saturated with porous material using homotopy perturbation method (HPM) restricted to an appropriate boundary conditions. Their results showed that the variations of chemical reaction, Darcy number, rarefaction and wall-ambient temperature parameters substantially dictate the fluid flow and volume flow rate respectively. Ojemer¹ and Hamza (2022) put forth a computational treatment of an Arrhenius kinetically propelled heat emission and absorption fluid in a microchannel. Ahmad and Jha (2015) conducted a numerical and an analytical investigations of the influence of heat transfer flow of an

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How to cite: Ojemer¹, G., Hamza, M. M., Tambuwal, B. H., Bello, I., & Shuaibu, A. (2023). Influence of Soret and Radial Magnetic Field on Natural Convection of a Chemically Reactive Fluid in an Upright Porous Annulus. *UMYU Scientifica*, 2(3), 108 – 120. <https://doi.org/10.56919/usci.2323.017>

exothermic chemical reacting fluids in an upstanding porous pipe. Their findings depict that heat transmission amount on pipe surfaces, whether transient or steady-state, increases with time. [Jha et al. \(2011a, 2011b\)](#) studied the time-dependent natural convection of an exothermic reaction fluid in an upright channel restricted to two immeasurable upright parallel plates as well as in a tube. They concluded that the amount of heat transmission and shear stress on both walls increases as the chemical reactant parameter is increased. References like [Ojmeri et al. \(2019\)](#), [Hamza et al. \(2019\)](#), [Ali et al. \(2014\)](#), [Hamza \(2016\)](#) shed more light on this phenomenon

As a result of recent scientific and technological achievements, annular space applications in industry and engineering have continued to gain a lot of attention. The fields of heat exchangers and oil and gas well drilling operations ([Jha et al. 2015](#)) provide such examples. Related studies on natural convection flows in an upstanding annulus can be found in other literature. [Joshi \(1987\)](#) modeled natural convection flow in upstanding annuli having two isothermal limits, one warmer than the other. The thermo-diffusion effect is the diffusion of mass as a result of a temperature gradient, and it can be significant when the flow region has large density differences. Further, this impact can be considerable when species are applied at the surface of a fluid region with a density less than the nearby fluid. The thermal diffusion factor has been used to separate isotopes as well as to combine gases with very light and medium molecular weights ([Sravanthi 2014](#)). [Ahmad et al. \(2017\)](#) studied the steady state mixed convective heat and mass transfer flow of an exothermic chemically reacting fluid in an upward porous conduit affected by Soret effect. According to their findings, the Soret effect and mixed convection had a remarkable impact on the fluid velocity in the pipe. [Kaladhar et al. \(2016\)](#) examined the radiation and thermal diffusion actions on mixed convection of a pair stress fluid between two permeable vertical plates. [Srinivasacharya and Kaladhar \(2013\)](#) inspected the thermos-diffusion and Dufour actions on the natural convection of a couple fluids in an upright channel with chemical interaction. In a separate study, [Srinivasacharya and Kaladhar \(2014\)](#) studied the chemical reactions, Soret, and Dufour factors on mixed convection flow between vertical parallel plates of a pair stress fluid. [Cheng \(2009\)](#) examined the thermal diffusion and Dufour impacts on natural convective heat and mass transport through a porous upstanding plate.

Investigators have in recent times beamed their searchlight on the analysis of magneto-hydrodynamics (MHD) due to its numerous possible implications it could have in astronomy, geophysics, and engineering. These assessments are essential in a number of industries, such as space vehicle technology, extraction processes, nuclear power facilities, and geothermal power generation. ([Vanita and Kumar 2016](#)). [Globe \(1959\)](#) was the first to present the annular MHD flow problem, concentrating on steady laminar hydromagnetic flow in an annular channel. Quite recently, [Yale et al. \(2023\)](#) investigated the impact of MHD

free convection of an incompressible fluid in the presence of viscous dissipation through a heated superhydrophobic microchannel. They concluded that the actions of viscous dissipation and super-hydrophobicity is seen to significantly encourage the fluid flow. [Taid and Ahmed \(2022\)](#) applied the perturbation technique to determine the consequences of the thermal diffusion, viscous dissipation, and chemical reaction on steady two-dimensional MHD free flow along an inclined permeable channel entrenched in a porous material. [Osman et al. \(2022\)](#) discussed the action of MHD on natural convection flow along an immeasurable inclined plate using the Laplace transformation approach. [Siva et al. \(2021\)](#) echoed the significance of hydromagnetic action on a heat transfer problem of electrokinetic flow in a rotational microfluidic channel. [Mozayyeni and Rahimi \(2012\)](#) investigated mixed convection in an upright annulus in the involvement of a radial magnetic field and they concluded that using an external magnetic field can successfully reduce fluid velocity and temperature. [Reddy and Reddy \(2009\)](#) studied the effects of radiation and mass transfer on the time-dependent hydromagnetic flow of an electrically-conducting fluid across a moving upright cylinder. They analyzed the flow patterns of momentum, energy, mass diffusion, drag force and rates of heat and mass transfers based on the fluctuations in the regulating thermo-physical and hydro-dynamical factors. Other works published to exemplify this concept include [Ali et al. \(2013\)](#), [Javaherdeh et al. \(2015\)](#), [Sankar et al. \(2006\)](#), to cite a few.

The purpose of this article is to basically modify the work conducted by [Ahmad et al. \(2017\)](#) by carrying out a steady state investigation of thermal diffusion and radial magnetic field effects on the free convection of a viscous reactive fluid in an upstanding porous annulus. The novelty of this work is in the fact that a different flow geometry was considered, ie, the porous annulus, which is a more effective tool for controlling heat transfer and fluid flow in both tall and shallow cavities. Moreover, the annulus model is a more general flow channel than the cylindrical pipe used in the the previous literature. When $\lambda \rightarrow \infty$, the annulus approaches a cylindrical pipe whereas when $\lambda \rightarrow 1$, the annulus behaves like two parallel plates. When the value of λ is in between, the curvature differences between the inner and outer walls can lead to various flow patterns. The formulated model is a set of nonlinear ordinary differential equations in terms of mass diffusion, energy and momentum, which has been solved semi-analytically by a regular perturbation approach with a power series expansion in the reactant consumption parameter λ . Shear stress, heat and mass transfer rates have also been calculated. Major parameters controlling the different flow patterns are graphically presented and discussed. The results of this investigation can find relevance in areas such as lubrication industries, chemical engineering, biomedical sciences, processing and drilling industries, and so forth.

MATERIALS AND METHODS

Mathematical Analysis

Figure 1 depicts the geometry of the current paper under discussion in schematic form. As illustrated in figure 1, we investigate a steady state free convection of chemically

reacting fluid with sores and a radial magnetic number in an upright permeable annulus of unlimited length. The fluid is thought to be Newtonian and obeys Boussinesq's approximation when immersed in it at a constant temperature T_0 . Following [Ahmad et al. \(2017\)](#) and [Hamza et al. \(2019\)](#), the dimensional form of the diffusion, temperature, and velocity equations under the aforementioned assumptions are:

$$\frac{\partial u'}{\partial t'} + \frac{v_0 b}{r'} \frac{\partial u'}{\partial r'} = \nu \left[\frac{\partial^2 u'}{\partial r'^2} + \frac{1}{r'} \frac{\partial u'}{\partial r'} \right] + g\beta(T' - T_0) + g\beta^*(\phi' - \phi_0) - \frac{\sigma\beta_0^2 b^*}{\rho r'} u' \tag{1}$$

$$\frac{\partial T'}{\partial t'} + \frac{v_0 b}{r'} \frac{\partial T'}{\partial r'} = \alpha \left[\frac{\partial^2 T'}{\partial r'^2} + \frac{1}{r'} \frac{\partial T'}{\partial r'} \right] + \frac{QC_0 A}{\rho C_p} \exp\left(-\frac{E}{RT'}\right) \tag{2}$$

$$\frac{\partial \phi'}{\partial t'} + \frac{v_0 b}{r'} \frac{\partial \phi'}{\partial r'} = D_m \left[\frac{\partial^2 \phi'}{\partial r'^2} + \frac{1}{r'} \frac{\partial \phi'}{\partial r'} \right] + \frac{D_m K_T}{T_m} \left[\frac{\partial^2 T'}{\partial r'^2} + \frac{1}{r'} \frac{\partial T'}{\partial r'} \right] \tag{3}$$

The initial and boundary conditions to be satisfied are:

$$\left. \begin{aligned} u' = 0, \theta' = \theta_0, \phi' = \phi_0 \text{ for } a^* \leq r' \leq b^* \\ \{ u' = 0, T' = T_w', \phi' = \phi_w' \text{ at } r' = a^* \} \\ \{ u' = 0, \theta' = 0, \phi' = 0 \text{ at } r' = b^* \} \end{aligned} \right\} \tag{4}$$

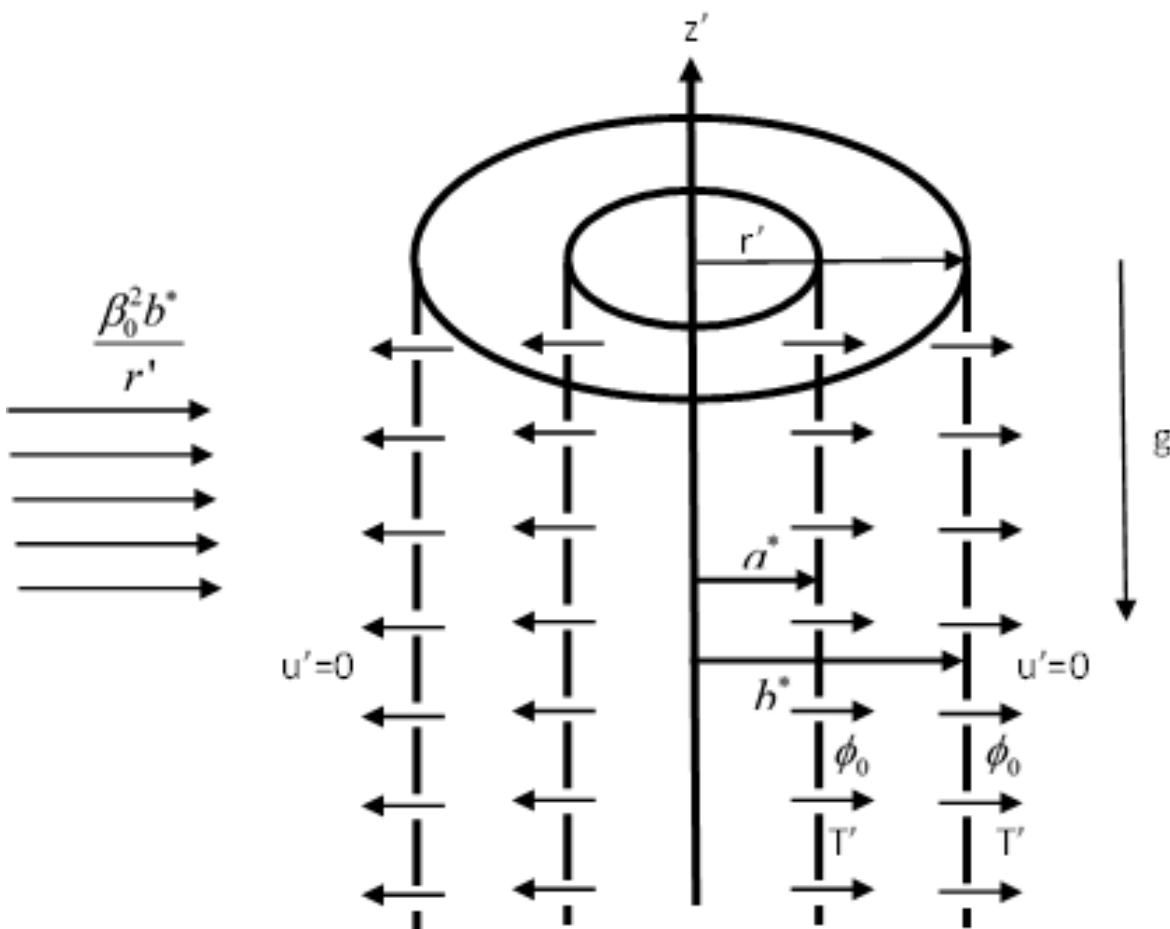


Fig. 1 Physical coordinate of the flow domain

we introduce the non-dimensional quantities:

$$\begin{aligned}
 u &= \frac{u'}{U_0}, t = \frac{t'v}{b^2}, \theta = \frac{E}{RT_0^2}(T'-T_0), \phi = \frac{E(\phi' - \phi_0)}{R\phi_0^2}, \lambda = \frac{QC_0AEb^2}{kRT_0^2} \exp\left(-\frac{E}{RT_0}\right), Sc = \frac{v}{D}, \\
 Sr &= \frac{D_m K_T (T_1 - T_0)}{vT_1(C_1 - C_0)}, N = \frac{\beta^*(\phi_1 - \phi_0)}{\beta(T_1 - T_0)}, M^2 = \frac{\sigma B_0^2 r_0^2}{\rho\nu}, b = \frac{b^*}{a^*}, \theta_a = \frac{E(T_w - T_0)}{RT_0^2} \\
 \varepsilon &= \frac{RT_0}{E}, r = \frac{r'}{b}, s = \frac{v_0 b}{v}, \phi_a = \frac{E(\phi_w - \phi_0)}{R\phi_0^2}
 \end{aligned} \tag{5}$$

Analytical Solutions

The steady state solutions for the reactive viscous fluid's concentration, temperature, and velocity fields, as well as shear stress, rates of heat and mass transfers, are obtained. When non-dimensional quantities are introduced, the closed-form resultant governing equations of this model become:

$$\frac{d^2u}{dr^2} + \frac{1}{r}(1-s)\frac{du}{dr} - \frac{M^2U}{r^2} + \theta + N\phi = 0 \tag{6}$$

$$\frac{d^2\theta}{dr^2} + \frac{1}{r}(1-sPr)\frac{d\theta}{dr} + \lambda \exp\left(\frac{\theta}{1+\varepsilon\theta}\right) = 0 \tag{7}$$

$$\frac{d^2\phi}{dr^2} + \frac{1}{r}(1-sSc)\frac{d\phi}{dr} = -Sr \left[\frac{d^2\theta}{dr^2} + \frac{1}{r} \frac{d\theta}{dr} \right] \tag{8}$$

Restricted to the boundary conditions below:

$$\begin{aligned}
 u = 0, \quad \theta = \theta_a, \quad \phi = \phi_a \quad \text{at} \quad r = 1 \\
 u = 0, \quad \theta = 0, \quad \phi = 0 \quad \text{at} \quad r = b
 \end{aligned} \tag{9}$$

Where M, s, Pr, Sc, Sr, λ, ε, θ_a, and φ_a are magnetic field, suction/injection, Prandlt number, Schmidt number, Soret number, chemical reacting parameter, activation energy, ambient temperature and ambient concentration parameters respectively.

Because the problem is extremely nonlinear, we used a regular perturbation technique with a power series expansion in the reactant consumption parameter λ.

$$\phi = \phi_0 + \lambda\phi_1 + \lambda^2\phi_2 + \lambda^3\phi_3 + O(\lambda) \tag{10}$$

$$\theta = \theta_0 + \lambda\theta_1 + \lambda^2\theta_2 + \lambda^3\theta_3 + O(\lambda) \tag{11}$$

$$U = u_0 + \lambda u_1 + \lambda^2 u_2 + \lambda^3 u_3 + O(\lambda) \tag{12}$$

inserting eqns (10) and (11) and (12) into eqns (6), (7) and (8) and comparing the coefficients of like powers of λ, the analytical solutions for the governing equations are obtained as follows:

$$U = \lambda [A_3 r^{z1} + A_4 r^{-z2} + B_3 r^2] + \lambda^2 [A_5 r^{z1} + A_6 r^{-z2} + B_7 r^4 + B_8 r^3 + B_9 r^2] + \lambda^3 [A_7 r^{z1} + A_8 r^{-z2} + B_{13} r^6 + B_{14} r^5 + B_{15} r^4 + B_{16} r^3 + B_{17} r^2] \tag{13}$$

$$\theta = x_4 (k_1 r + k_2) + \lambda [x_2 (2k_3 r + 2k_4 - r^2)] + \lambda^2 \left[x_4 x_2 \left(\frac{r^4}{12} - \frac{k_3 r^3}{3} - k_4 r^2 \right) + x_4 (k_5 r + k_6) \right] + \lambda^3 \left[\left\{ x_4^2 x_2 \left(\frac{k_4 r^4}{12} + \frac{k_3 r^5}{60} - \frac{r^6}{360} \right) - x_4^2 \left(\frac{k_5 r^3}{6} + \frac{k_6 r^2}{2} \right) \right\} + x_1 x_3 x_4 \left(\frac{r^6}{30} - \frac{k_3 r^5}{5} - \frac{k_4 r^4}{3} + \left(\frac{k_3^2 r^4}{3} + \frac{4k_3 k_4 r^3}{3} + 2k_4^2 r^2 \right) + x_4 (k_7 r + k_8) \right] \tag{14}$$

$$\phi = -x_5 Sr (x_4 k_1 (r \ln(r) - r)) + x_5 (k_9 r + k_{10}) + \lambda [-x_5 Sr (2x_2 k_3 (r \ln(r) - r) - 2x_2 r^2) + x_5 (k_{11} r + k_{12})] + \lambda^2 \left[-x_5 Sr \left\{ x_4 x_2 \left(\frac{r^4}{9} - \frac{k_3 r^3}{2} - 2k_4 r^2 \right) + x_4 k_5 (r \ln(r) - r) \right\} + x_5 (k_{13} r + k_{14}) \right] + \lambda^3 \left[-x_5 Sr \left\{ x_4^2 x_2 \left(\frac{k_4 r^4}{9} + \frac{k_3 r^5}{48} - \frac{r^6}{300} \right) - x_4^2 \left(\frac{k_5 r^3}{4} + k_6 r^2 \right) \right\} + x_1 x_3 x_4 \left(\frac{r^6}{25} - \frac{k_3 r^5}{4} - \frac{4k_4 r^4}{9} + \frac{4k_3^2 r^4}{9} + 2k_3 k_4 r^3 + 4k_4^2 r^2 \right) + x_4 k_7 (r \ln(r) - r) \right\} + x_5 (k_{15} r + k_{16}) \tag{15}$$

The skin frictions on the boundaries are:

$$\tau_1 = \frac{dU}{dr} \Big|_{r=1} = \lambda (z1A_3 - z2A_4 + 2B_3) + \lambda^2 (z1A_5 - z2A_6 + 4B_6 + 3B_7 + 2B_8) + \lambda^3 (z1A_7 - z2A_8 + 6B_{11} + 5B_{12} + 4B_{13} + 3B_{14} + 2B_{15}) \tag{16}$$

$$\tau_b = \frac{dU}{dr} \Big|_{r=b} = \lambda (z1A_3 b^{z1-1} - z2A_4 b^{-z2-1} + 2B_3 b) + \lambda^2 (z1A_5 b^{z1-1} - z2A_6 b^{-z2-1} + 4B_6 b^3 + 3B_7 b^2 + 2B_8 b) + \lambda^3 (z1A_7 b^{z1-1} - z2A_8 b^{-z2-1} + 6B_{11} b^5 + 5B_{12} b^4 + 4B_{13} b^3 + 3B_{14} b^2 + 2B_{15} b) \tag{17}$$

The mass and heat transfer on both boundaries is equal, attributable to the uniform nature of the flow, and as a result, the steady-state rates of heat and mass transfers on the boundaries are derived as follows:

$$Nu = \frac{d\theta}{dr} \Big|_{r=b} = x_4 k_1 + \lambda [2x_2 (k_3 - b)] + \lambda^2 \left[x_4 x_2 \left(\frac{b^3}{3} - k_3 b^2 - 2k_4 b \right) + x_4 k_5 \right] + \lambda^3 \left[x_4^2 x_2 \left(\frac{k_4 b^3}{3} + \frac{k_3 b^4}{12} - \frac{b^5}{60} \right) - x_4^2 \left(\frac{k_5 b^2}{2} + k_6 b \right) + x_1 x_3 x_4 \left(\frac{b^5}{5} - k_3 r^4 - \frac{4k_4 b^4}{3} + \frac{4k_3^2 b^3}{3} - 4k_3 k_4 b^2 + 4k_4^2 b \right) + x_4 k_7 \right] \tag{18}$$

$$\begin{aligned}
 Sh = \frac{d\phi}{dr} \Big|_{r=b} &= \left[-x_5 x_4 k_1 Sr (In(b)) \right] + x_5 k_9 + \lambda \left[-x_5 Sr (2x_2 k_3 In(b) - 4x_2) + x_5 k_{11} \right] + \\
 &\lambda^2 \left[-x_5 Sr \left\{ x_4 x_2 \left(\frac{4b^3}{9} - \frac{3k_3 b^2}{2} - 4k_4 b \right) + x_4 k_5 In(b) \right\} + x_5 k_{13} \right] + \lambda^3 \left[x_5 Sr \left\{ x_4^2 x_2 \left(\frac{4k_4 b^3}{9} - \frac{5k_3 b^4}{48} \right. \right. \right. \\
 &\left. \left. \left. - \frac{b^5}{50} \right) - x_5 Sr \left(\frac{3k_5 b^2}{4} + 2k_6 b \right) + x_1 x_3 x_4 \left(\frac{6b^5}{25} - \frac{5k_3 b^4}{4} - \frac{16k_4 b^3}{9} + \frac{16k_3^2 b^3}{9} + 6k_3 k_4 b^2 + 8k_4^2 b \right) \right. \right. \\
 &\left. \left. + x_4 k_7 In(b) \right\} + x_5 k_{15} \right] \tag{19}
 \end{aligned}$$

where $x_1, x_2, x_3, x_4, x_5, k_1, k_2, k_3, k_4, k_5, k_6, k_7, k_8, k_9, k_{10}, k_{11}, k_{12}, k_{13}, k_{14}, k_{15}, k_{16}, A_3, A_4, A_5$

$A_6, A_7, A_8, B_3, B_7, B_8, B_9, B_{13}, B_{14}, B_{15}, B_{16}, B_{17}$ are indicated in the appendix.

RESULTS AND DISCUSSION

The natural convection of a hydromagnetic chemical reacting fluids with Soret and radial magnetic field effects is investigated in an upright permeable annulus. We have shown the impacts of pertinent parameters like Frank-Kamenetskii (λ), Sustentation (N), Soret number (Sr), and magnetic number (M) on the flow configurations in Fig. 2-15, using the default values of $\lambda=0.001$, $Sr=1$, $Sc=0.22$, $\epsilon=0.01$, $Pr=0.71$, $s=3$, $\theta_a=1$, $\phi_a=1$.

The influence of λ on temperature, concentration, and velocity distributions are depicted in Figures 2-4. These graphs show that as λ grows the temperature, concentration, and velocity of the fluid grow. This is owing to the truth that a growth in λ , which basically denotes the viscous heating parameter, corresponds to an increase in the chemical reaction's strength. Naturally speaking, these results make sense, as raising the heat source parameter indicates more heat generation from the region's surface, making the fluid to accelerate faster, thereby resulting in high performance of the system. There are many thermal applications where this result can find relevance which include power generation, space heating, cooking and industrial processes, to mention a few. These results corroborate with those obtained by Obalalu *et al.* (2021) and Hamza (2016). The actions of Soret on concentration and velocity gradients can be seen in Figures 5 and 6. As can be seen from these graphs, increasing the value of Sr increases the fluid's concentration and velocity. This is physically true because the effect of Soret number appears in suspended mixture of particles and fluid and this phenomenon is made available by temperature gradients, consequently, the transport of fluid molecule in the highest energy level moves the particles to coldest region. This concept is very applicable in chemical and petroleum engineering processes as asserted by Ahammad and Krishna (2021). The effect of Sc on concentration is shown in Fig. 7, and it is clear that as the Schmidt number increases, the mass flux decreases. Figures 8–10 show the impacts of Pr , M , and N on the fluid flow. As illustrated in these graphs, increasing the Pr and M parameters decreases fluid flow.

The fact that $M = 0$ implies that the flow is totally hydrodynamic and that there is no magnetic effect. As the value of M grows, the velocity drops, as demonstrated in this diagram. This is to be expected, as the Lorentz force, which is a resistance-type force, is always produced when a transverse magnetic field is introduced. When M grows, the drag force tends to resist the fluid motion, leading to a considerable reduction in fluid speed. On the other hand, increases in N boost up the velocity of the flow, which also coincide with the findings of Hamza *et al.* (2019).

Figures 11-14 show the effects of varying frictional factor levels at the isothermal boundary at $r = 1$ (at the external wall of the inner cylinder) and $r = b$ (at the inner surface of the outer cylinder). Figure 11 depicts the effect of λ and Sr on the shear stress. At $r = 1$, increasing λ and Sr strengthens the drag force, but at $r = b$, increasing λ and Sr decreases the drag force as portrayed in (Figure 11b). Raising the levels of both λ and M reduces the shear stress for $r = 1$, as shown in Figure 12a, but for $r = b$, the opposite occurs, as shown in Figure 12b. Figure 13 depicts the impacts of λ and Pr on the frictional factors. When $r = 1$, increasing the Prandtl number causes skin friction to increase, whereas increasing the value of λ causes skin friction to decrease. Figure 13b shows the opposite at $r = b$. Figure 14a shows that skin friction increases as both λ and N climb. When $r = b$, however, as illustrated in Figure 14b, the opposite is true. The influence of Sr and Pr on Nusselt number and Sherwood number, respectively, against λ is depicted in Figure 15. Raising the value of Pr reduces the rate of heat transmission, whereas increasing the value of λ increases the rate of heat transfer, as illustrated in Figure 15a. Physically, as λ rises, the fluid temperature rises with it, as does the temperature gradient, resulting in a faster heat transfer rate. The influence of λ and Sr on the mass transfer rate is depicted in Figure 15b. As indicated in the figure, increasing both λ and Sr yealds a larger mass transfer flow.

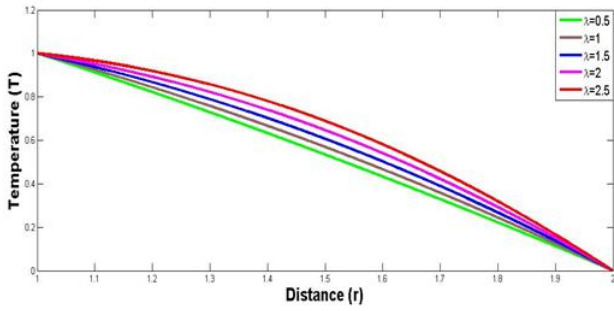


Figure 2 λ on temperature profile

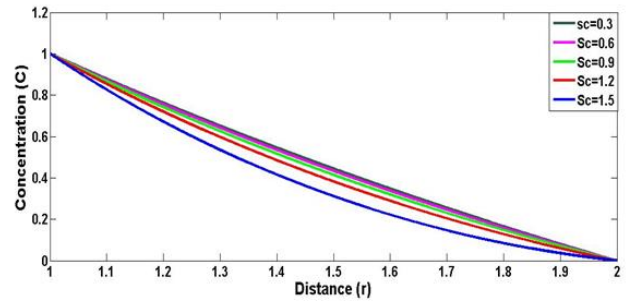


Figure 7 Sc on Concentration profile

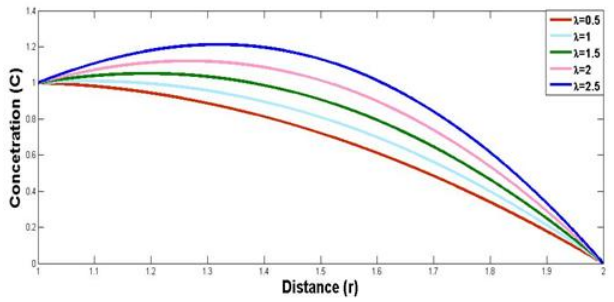


Figure 3 λ on Concentration profile

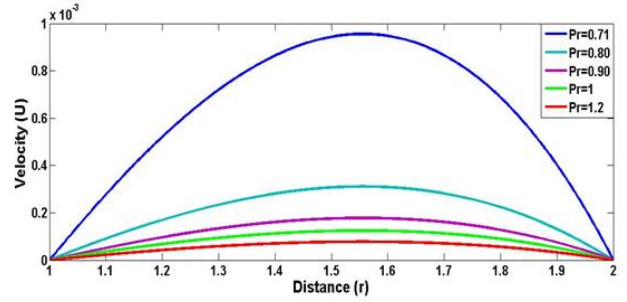


Figure 8 Pr on Velocity profile

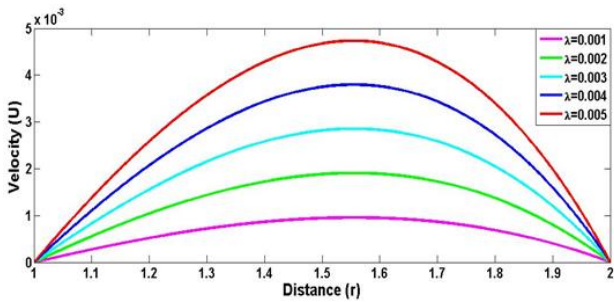


Figure 4 λ on Velocity profile

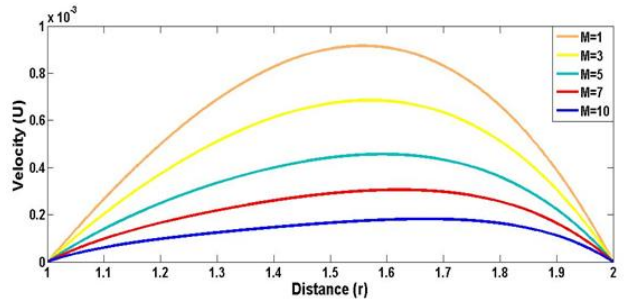


Figure 9 M on Velocity profile

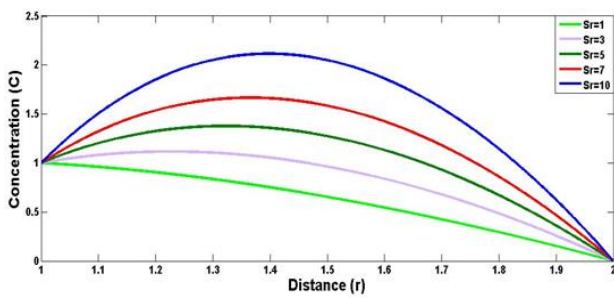


Figure 5 Sr on Concentration profile

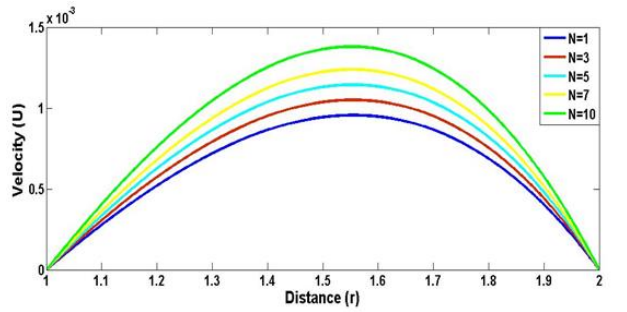


Figure 10 N on Velocity profile

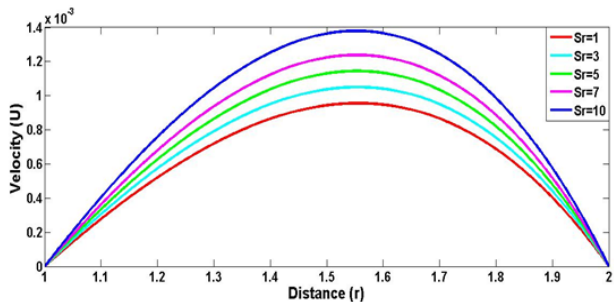


Figure 6 Sr on Velocity profile

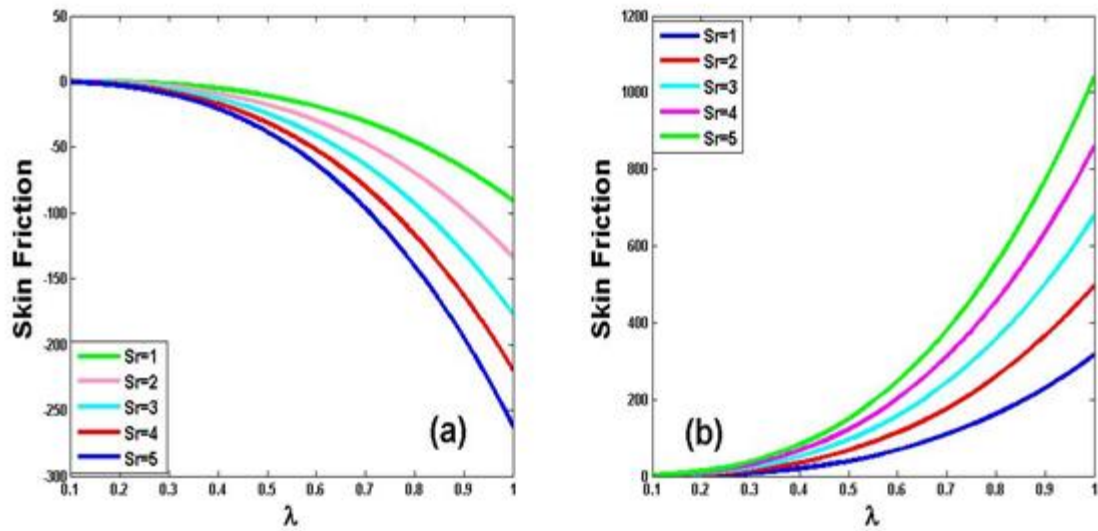


Figure 11 Sr on Skin friction

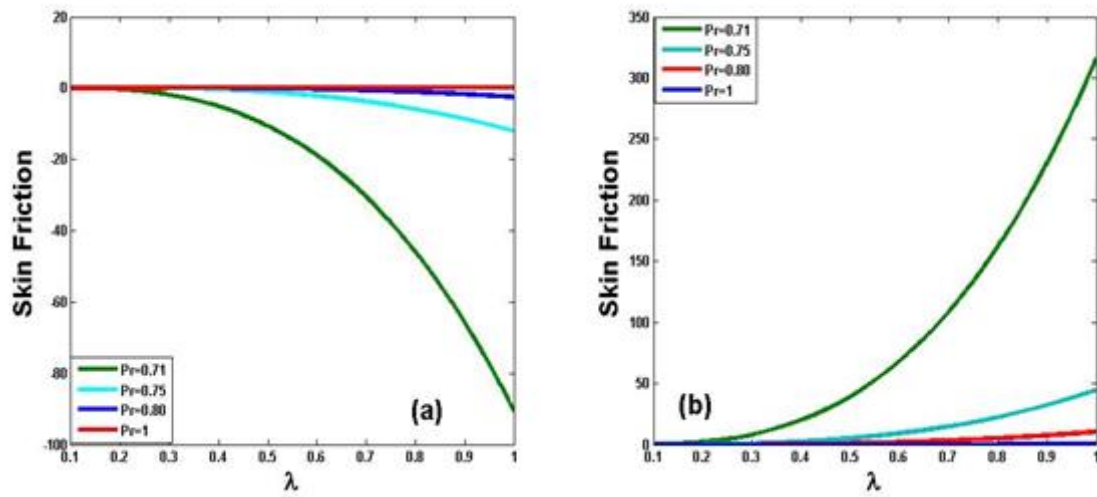


Figure 12 Pr on Skin friction

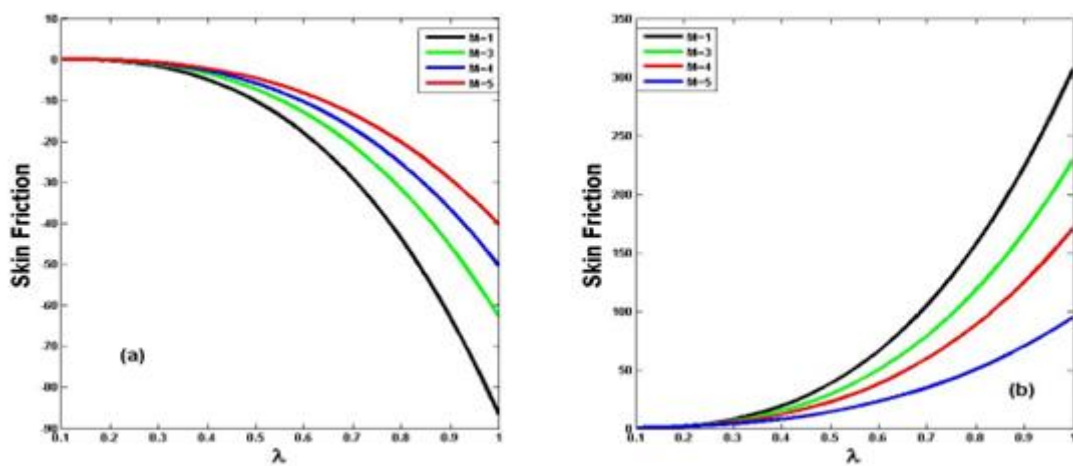


Figure 13 M on Skin friction

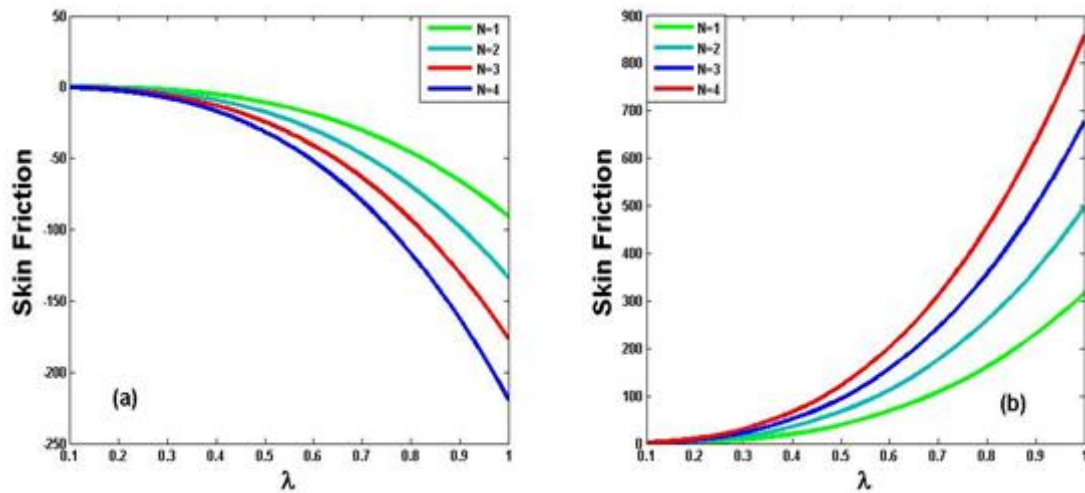


Figure 14 N on Skin friction

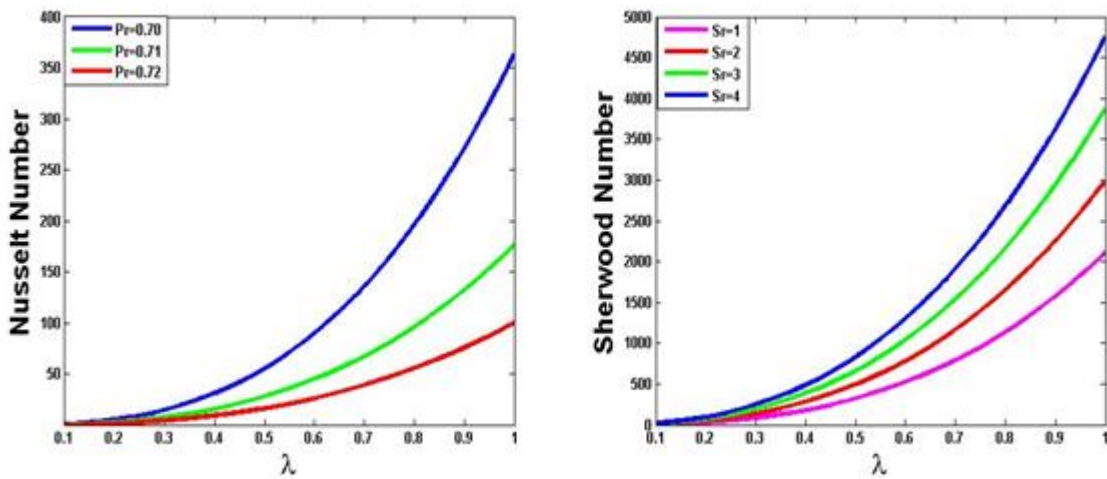


Figure 15 Pr and Sr against λ on Nusselt number and Sherwood number

CONCLUSIONS

In this study, we analyze the steady-state hydromagnetic flows for mass diffusion, temperature, momentum, shear stress, Nusselt, and Sherwood numbers in an upright permeable annulus for chemical reacting fluids affected by Soret and radial magnetic field impacts. Using a perturbation series technique, we determine the nonlinear steady state governing equations analytically. We examine the impacts of Frank-Kamenetskii (λ), sustentation (N), thermos-diffusion (Sr), and radial magnetic field (M) on flow configuration. Our findings suggest that increasing the values of Frank–Kamenetskii, sustentation, and thermal diffusion parameters improves the speed of the

fluid, while higher values of radial magnetic field slow down the fluid flow. Furthermore, we observe that stronger temperature and concentration gradients lead to increased amounts of heat and mass transfer flow, respectively. The outcomes of this research correspond to those found in previously published results such as that of *Ahmad et al. (2017)* and *Hamza et al. (2019)*. In practical situations, the annular geometry is a more useful mechanism for heat exchangers, which is typically used for gas cooled nuclear reactors as well as in drilling activities of oil and gas wells. Also, the Soret effect has been used as a means of isotope separation and in a mixture of gases of very light and medium molecular weights. In the future, this study can be expanded to investigate the effect of time as well as the action of chemical reaction.

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APPENDIX

All the Constants used During the Analytical Solutions are Defined here:

$$\begin{aligned}
 x_1 &= e^{-\frac{1}{2}}, x_2 = \frac{1}{4-2sPr}, x_3 = \frac{1}{(2-sPr)^2}, x_4 = \frac{1}{2-sPr}, x_5 = \frac{1}{2-sSc}, z_1 = \frac{s+\sqrt{s^2+4M^2}}{2}, z_2 = \frac{-s+\sqrt{s^2+4M^2}}{2} \\
 k_1 &= \frac{2-sPr}{1-b}, k_2 = -k_1b, k_3 = \frac{b^2-1}{2(b-1)}, k_4 = \frac{b^2}{2} - k_3b, k_5 = \frac{x_2}{b-1} \left\{ k_4(b^2-1) + \frac{k_3(b^3-1)}{3} + \frac{(1-b^4)}{12} \right\} \\
 k_6 &= x_2 \left(k_4b^2 + \frac{k_3b^3}{3} - \frac{b^4}{12} \right) - k_3b, k_7 = \frac{1}{b-1} \left[x_2 \left\{ x_2 \left(\frac{b^6-1}{360} \right) + k_3 \left(\frac{1-b^5}{60} \right) + k_4 \left(\frac{1-b^4}{12} \right) + \right. \right. \\
 &\left. \left. \frac{k_5(b^3-1)}{6} + \frac{k_6(b^2-1)}{2} \right\} + x_1x_3 \left(\frac{1-b^6}{30} + \frac{k_3(b^5-1)}{5} + \frac{k_4(b^4-1)}{3} + \frac{k_3^2(1-b^4)}{3} + \frac{4k_3k_4(1-b^3)}{3} + 2k_4^2(1-b^2) \right) \right] \\
 k_8 &= \left[x_2 \left\{ x_2 \left(\frac{b^6}{360} \right) - k_3 \frac{b^5}{60} - k_4 \frac{b^4}{12} + \right. \right. \\
 &\left. \left. \frac{k_5b^3}{6} + \frac{k_6b^2}{2} \right\} - x_1x_3 \left(\frac{b^6}{30} - \frac{k_3b^5}{5} - \frac{k_4b^4}{3} + \frac{k_3^2b^4}{3} + \frac{4k_3k_4b^3}{3} + 2k_4^2b^2 \right) - k_7b \right] \\
 k_9 &= \frac{Sr}{b-1} \{ x_4k_1(1+b \log b - b) \} - \frac{2+sSc}{b-1}, k_{10} = Sr \{ x_4k_1(1+b \log b - b) \} - k_9b \\
 k_{11} &= \frac{Sr}{2-sSc} \{ 2x_2k_3(1+b \log b - b) + 2x_2(1-b^2) \}, k_{12} = Sr \{ 2x_2k_3(1+b \log b - b) + 2x_2(1-b^2) \} - k_{11}b \\
 k_{13} &= \frac{Sr}{b-1} \left[x_4x_2 \left(\frac{b^4-1}{9} + \frac{k_3(1-b^3)}{2} + 2k_4(1-b^2) + x_4k_5(1+b \log b - b) \right) \right] \\
 k_{14} &= Sr \left[x_4x_2 \left(\frac{b^4}{9} + \frac{k_3b^3}{2} + 2k_4b^2 + x_4k_5(b \log b - b) \right) \right] - k_{13} \\
 k_{15} &= \frac{Sr}{b-1} \left[x_4^2 \left\{ x_2 \left(\frac{k_4(1-b^4)}{9} + \frac{5k_3(1-b^5)}{48} + \frac{b^6-1}{300} \right) - k_5 \frac{(1-b^3)}{6} - k_6(1-b^2) \right. \right. \\
 &\left. \left. x_1x_3x_4 \left(\frac{1-b^6}{50} + \frac{k_3(b^5-1)}{4} + \frac{4k_4(b^4-1)}{9} + \frac{4k_3^2(1-b^4)}{9} + 2k_3k_4(1-b^3) + 4k_4^2(1-b^2) \right) \right. \right. \\
 &\left. \left. x_4k_7(1+b \log b - b) \right\} \right] \\
 k_{16} &= Sr \left[x_4^2 \left\{ x_2 \left(\frac{k_4b^4}{9} + \frac{5k_3b^5}{48} - \frac{b^6}{300} \right) - k_5 \frac{b^3}{4} - k_6b^2 \right. \right. \\
 &\left. \left. x_1x_3x_4 \left(\frac{2b^6}{50} - \frac{k_3b^5}{4} - \frac{4k_4(b^4)}{9} + \frac{4k_3^2(b^4)}{9} + 2k_3k_4(b^3) + 4k_4^2(b^2) \right) \right. \right. \\
 &\left. \left. x_4k_7(1+b \log b - b) \right\} \right] - k_{15}b
 \end{aligned}$$

$$\begin{aligned} \eta_8 &= -2x_2k_4, \eta_{12} = -Nx_5k_{12}, \eta_{15} = x_2x_4k_4, \eta_{16} = -x_4k_5, \eta_{17} = -x_4k_6, \eta_{20} = -NSrx_2x_4x_5k_4, \eta_{24} = -NSrx_4x_5k_5 \\ \eta_{25} &= -Nx_5k_{13}, \eta_{26} = -Nx_5k_{14}, \eta_{27} = \frac{-x_4^2x_2k_4}{12}, \eta_{30} = \frac{-x_4^2k_5}{12}, \eta_{31} = \frac{-x_4^2k_6}{2}, \eta_{32} = x_1x_3x_4, \eta_{35} = \frac{-\eta_{32}k_4}{3}, \eta_{36} = \frac{\eta_{32}k_3^2}{3} \\ \eta_{37} &= \frac{-4\eta_{32}k_3k_4}{3}, \eta_{38} = 2\eta_{32}k_4^2, \eta_{39} = -x_4k_7, \eta_{40} = -x_4k_8, \eta_{41} = \frac{-NSrx_4^2x_2x_5k_4}{12}, \eta_{44} = \frac{-NSrx_5x_4^2k_5}{6}, \eta_{45} = \frac{-NSrx_5x_4^2k_6}{2} \\ \eta_{48} &= N\eta_{35}Srx_5, \eta_{49} = N\eta_{36}Srx_5, \eta_{50} = N\eta_{37}Srx_5, \eta_{51} = N\eta_{38}Srx_5, \eta_{52} = \frac{-NSrx_4^2x_2x_5k_4}{36}, \eta_{55} = \frac{-NSrx_4^2x_5k_5}{12}, \\ \eta_{56} &= \frac{-NSrx_4^2x_5k_6}{2}, \eta_{60} = \frac{N\eta_{32}Srx_5k_3^2}{9}, \eta_{61} = \frac{2NSrx_5k_3k_4}{2}, \eta_{62} = 2\eta_{32}NSrx_5k_4^2, \eta_{63} = NSrx_5x_4k_7(\log(r) - r) \\ \eta_{64} &= -Nx_5k_{15}, \eta_{65} = -Nx_5k_{16} \end{aligned}$$

$$B_3 = \frac{\eta_8 + \eta_{12}}{2 + 2(1-s) - M^2}, B_7 = \frac{\eta_{15} + 2\eta_{20}}{12 + 4(1-s) - M^2}, B_8 = \frac{\eta_{16} + \eta_{24} + \eta_{25}}{6 + 3(1-s) - M^2}$$

$$B_9 = \frac{\eta_{16} + \eta_{26}}{2 + 2(1-s) - M^2}, B_{13} = \frac{\eta_{27} + \eta_{35} + \eta_{36} + \eta_{41} + \eta_{48} + \eta_{49} + \eta_{52} + \eta_{60}}{30 + 6(1-s) - M^2}$$

$$B_{14} = \frac{\eta_{30} + \eta_{37} + \eta_{44} + \eta_{50} + \eta_{55} + \eta_{61}}{20 + 5(1-s) - M^2}, B_{15} = \frac{\eta_{31} + \eta_{38} + \eta_{45} + \eta_{51} + \eta_{56} + \eta_{62}}{12 + 4(1-s) - M^2}$$

$$B_{16} = \frac{\eta_{39} + \eta_{63} + \eta_{64}}{6 + 3(1-s) - M^2}, B_{17} = \frac{\eta_{40} + \eta_{65}}{2 + 2(1-s) - M^2}, A_3 = -(A_4 + B_3),$$

$$A_4 = \frac{B_3}{b^{z1} - b^{-z2}}(b^2 + b^{z1}), A_5 = -(A_6 + B_7 + B_8 + B_9),$$

$$A_6 = \frac{1}{b^{z1} - b^{-z2}} \{ B_7(b^4 - b^{z1}) + B_8(b^3 - b^{z1}) + B_9(b^2 - b^{z1}) \},$$

$$A_7 = -(A_8 + B_{13} + B_{14} + B_{15} + B_{16} + B_{17}), A_8 = \frac{1}{b^{z1} - b^{-z2}} \{ B_{13}(b^6 - b^{z1}) + B_{14}(b^5 - b^{z1}) + B_{15}(b^4 - b^{z1})$$

$$B_{16}(b^3 - b^{z1}) + B_{17}(b^2 - b^{z1}) \}$$